Ordering number: EN 2307

Thick Film Hybrid IC

SANYO No.2307

STK4231II

2-Channel 100W min AF Power Amp (Dual Supplies)

Features

- The STK4201II series (STK4231II) and STK4201V series (high-grade type) are pin-compatible in the output range of 60W to 100W. Once the PCB pattern is designed, you can easily satisfy the requirements for new sets simply by changing the IC.
- Built-in muting circuit to cut off various kinds of pop noise
- Greatly reduced heat sink due to case temperature 125°C guaranteed
- Excellent cost performance

Maximum Ratings at Ta = 25°C

				unit
Maximum Supply Voltage	V_{CC} max		±75	V
Thermal Resistance	θj-c		1.1	°C/W
Junction Temperature	Tj		150	°C
Operating Case Temperature	T_C		125	°C
Storage Temperature	Tstg		−30 to +125	°C
Available Time for Load Shorted	t_s	V_{CC} = ±51.0V, R_L = 8Ω, f = 50Hz, Po = 100W	1	S

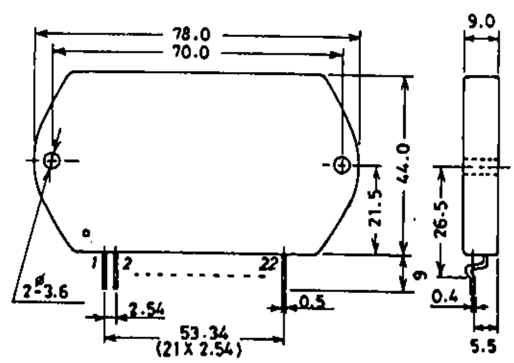
Recommended Operating Conditions at Ta = 25°C

			unit
Recommended Operating Voltage	V_{CC}	±51.0	V
Load Resistance	R_L	8	Ω

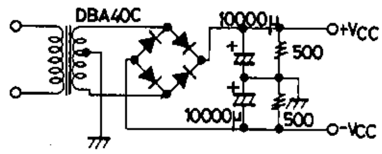
Operating Characteristics at Ta = 25°C, V_{CC} = ±51.0V, R_L = 8Ω, Rg = 600Ω, VG = 40dB, R_L : non-inductive load

			min	typ	max	unit
Quiescent Current	Icco	V_{CC} = ±60V	20	40	100	mA
Output Power	Po	THD = 0.4%, f = 20Hz to 20kHz	100			W
Total Harmonic Distortion	THD	Po = 1.0W, f = 1kHz			0.3	%
Frequency Response	f	Po = 1.0W, $\pm^{0}_{3}$ dB		20 to 50k		Hz
Input Resistance	r_i	Po = 1.0W, f = 1kHz		55		kΩ
Output Noise Voltage	V_{NO}	V_{CC} = ±60V, Rg = 10kΩ			1.2	mVrms
Midpoint Voltage	V_N	V_{CC} = ±60V	−70	0	+70	mV
Muting Voltage	V_M		−2	−5	−10	V

Package Dimensions 4086
(unit: mm)



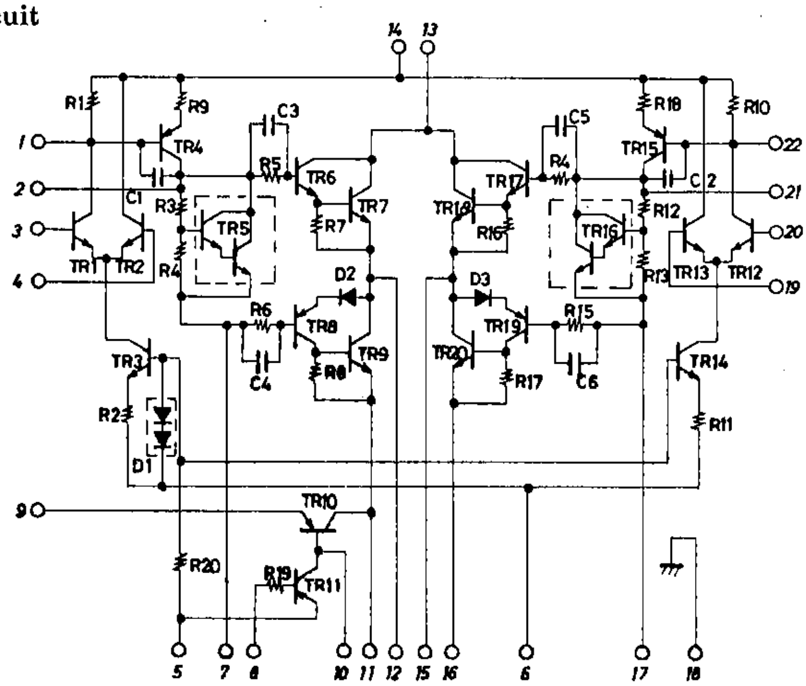
Note) · For power supply at the time of test, use a constant-voltage power supply unless otherwise specified.
· For measurement of the available time for load shorted and output noise voltage, use the specified transformer power supply shown right.
· The output noise voltage is represented by the peak value on rms scale (VTVM) of average value indicating type. For AC power supply, use an AC stabilized power supply (50Hz) to eliminate the effect of flicker noise in AC primary line.



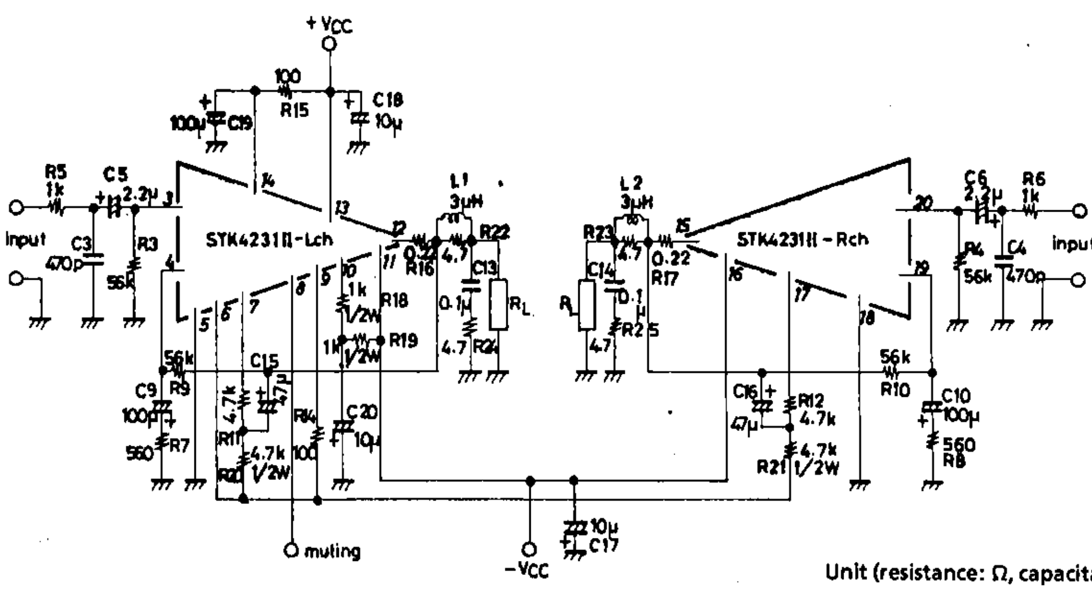
Specified Transformer Power Supply
(Equivalent to MG-200)

Unit (resistance: Ω, capacitance: F)

Equivalent Circuit

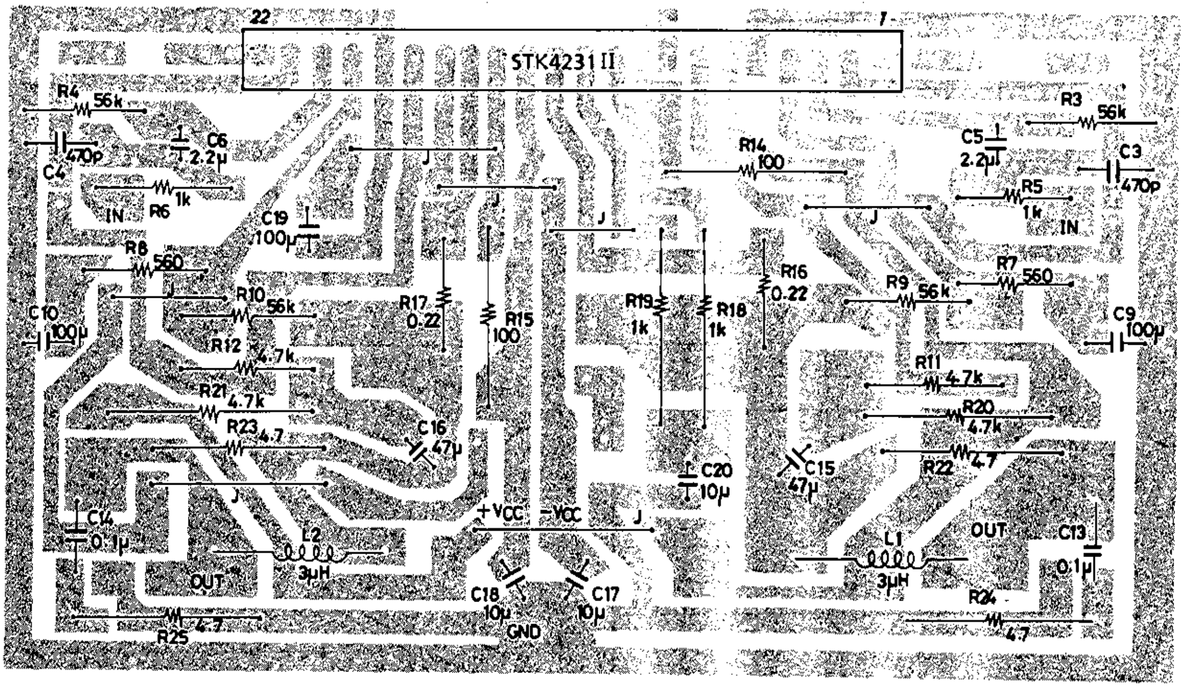


Sample Application Circuit: 100W min 2-channel AF power amp

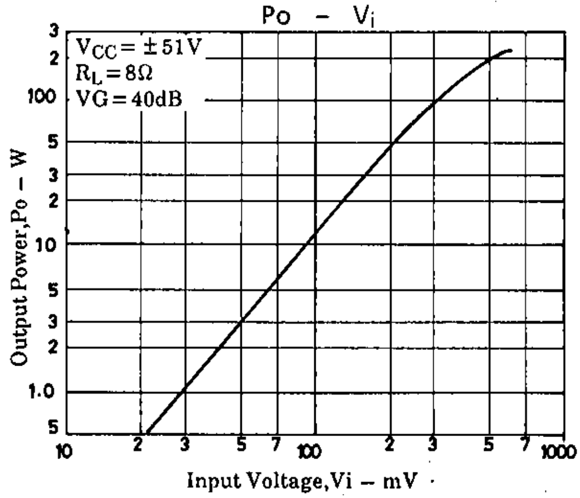


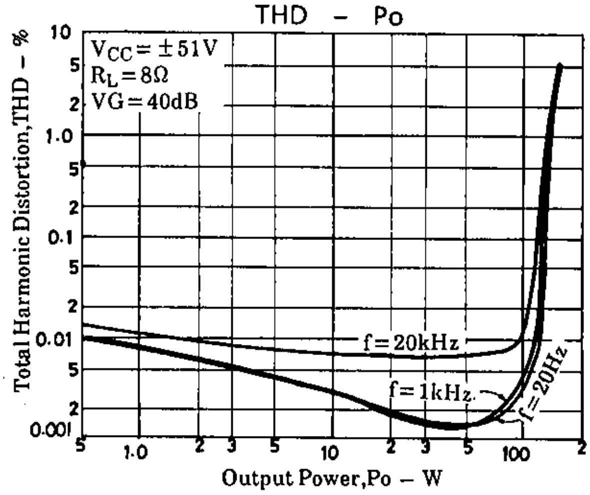
Unit (resistance: Ω, capacitance: F)

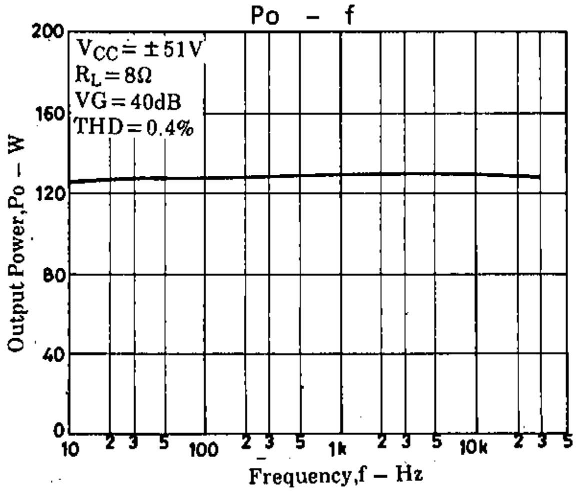
Sample Printed Circuit Pattern for Application Circuit (Cu-foiled side)

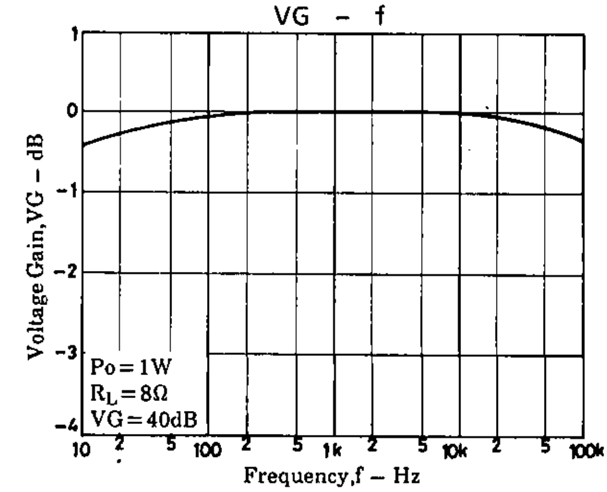


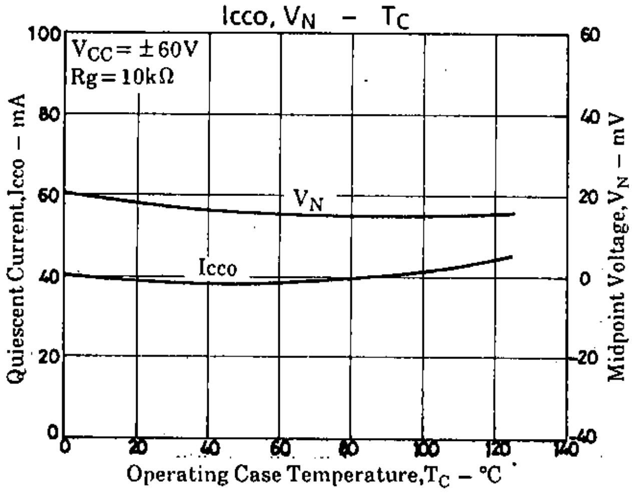
Unit (resistance: Ω, capacitance: F)

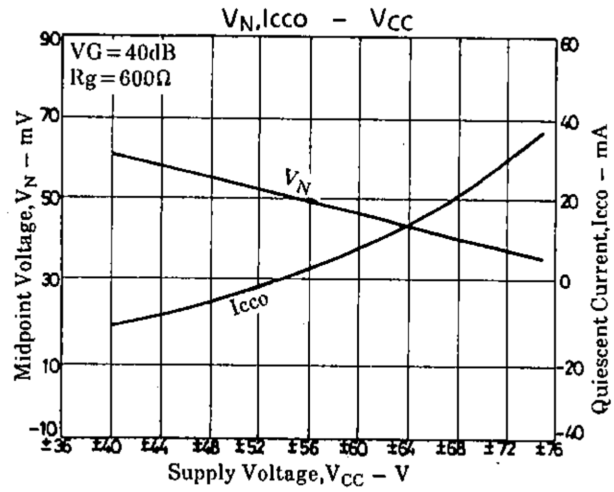


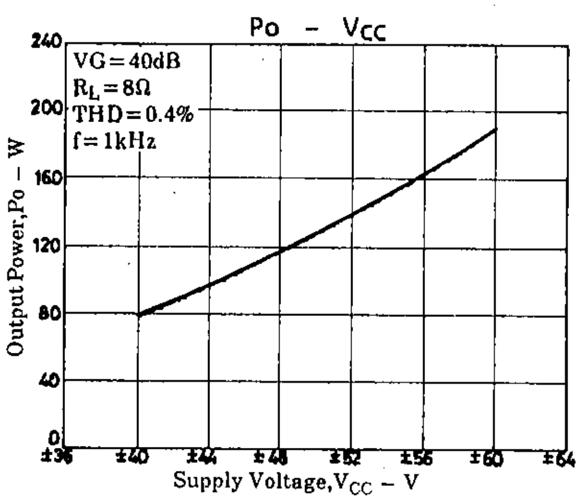


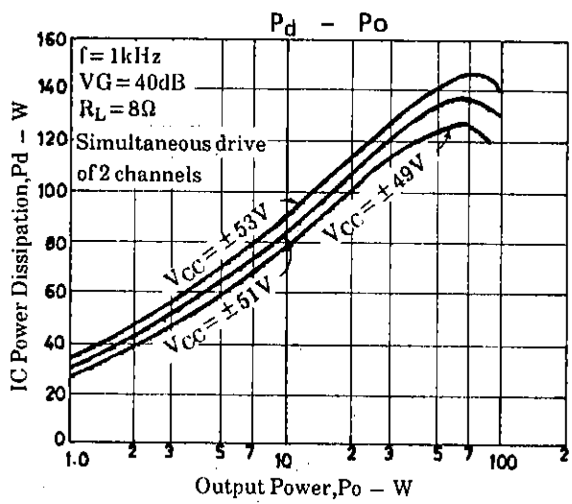


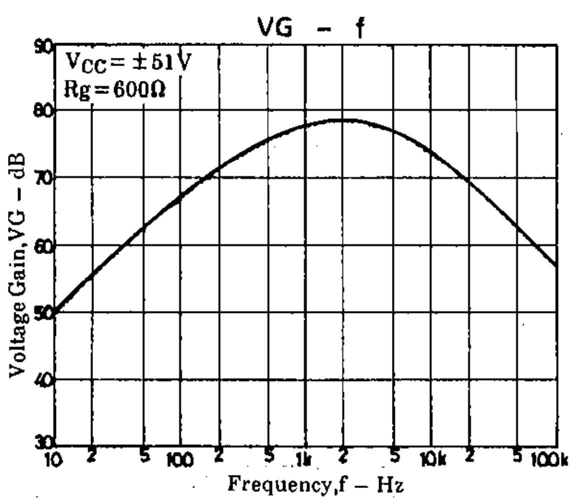



Icco, VN – TC
VCC=±60V
Rg=10kΩ
VN
Icco
Quiescent Current,Icco – mA
Midpoint Voltage,VN – mV
Operating Case Temperature,TC – °C

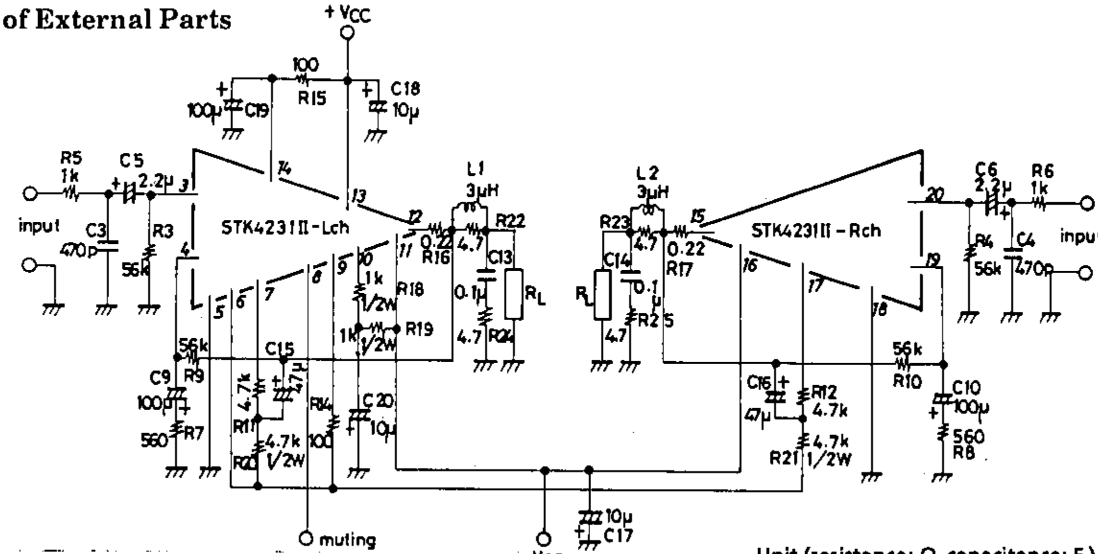

VN,Icco – VCC
VG=40dB
Rg=600Ω
VN
Icco
Midpoint Voltage,VN – mV
Quiescent Current,Icco – mA
Supply Voltage,VCC – V


Po – VCC
VG=40dB
RL=8Ω
THD=0.4%
f=1kHz
Output Power,Po – W
Supply Voltage,VCC – V


Pd – Po
f=1kHz
VG=40dB
RL=8Ω
Simultaneous drive
of 2 channels
VCC=±53V
VCC=±51V
VCC=±49V
IC Power Dissipation,Pd – W
Output Power,Po – W


VG – f
VCC=±51V
Rg=600Ω
Voltage Gain,VG – dB
Frequency,f – Hz

Description of External Parts



C3, C4 : Input filter capacitors
- A filter formed with R5 or R6 can be used to reduce noise at high frequencies.

C5, C6 : Input coupling capacitors
- Used to block DC current. When the reactance of the capacitor increases at low frequencies, the dependence of 1/f noise on signal source resistance causes the output noise to worsen. It is better to decrease the reactance.
- To reduce the pop noise at the time of application of power, it is effective to increase C5, C6 that fix the time constant on the input side and to decrease C9, C10 on the NF side.

C9, C10 : NF capacitors
- These capacitors fix the low cutoff frequency as shown below.

$$f_L = \frac{1}{2\pi \cdot C9 \cdot R7} \quad [\mathrm{Hz}]$$

To provide the desired voltage gain at low frequencies, it is better to increase C9. However, do not increase C9 more than needed because the pop noise level becomes higher at the time of application of power.

C19 : Decoupling capacitor
- Used to eliminate the ripple components that mix into the input side from the power line ($+V_{CC}$).

C15, C16 : Bootstrap capacitors
- When the capacitor value is decreased, the distortion is liable to be higher at low frequencies.

C17, C18 : Oscillation blocking capacitors
- Must be inserted as close to the IC power supply pins as possible so that the power supply impedance is decreased to operate the IC stably.
- Electrolytic capacitors are recommended for C17, C18.

C20 : Capacitor for ripple filter
- Capacitor for the TR10-used ripple filter in the IC system

C13, C14 : Oscillation blocking capacitors
- A polyester film capacitor, being excellent in temperature characteristic, frequency characteristic, is recommended for C13, C14.

R5, R6 : Resistors for input filter

R3, R4 : Input bias resistors
- Used to bias the input pin potential to zero. These resistors fix the input impedance practically.

R7, R9 : (R8, R10) These resistors fix voltage gain VG.
It is recommended to use R7 (R8) = 560Ω, R9 (R10) = 56kΩ for VG = 40dB.
- To adjust VG, it is desirable to change R7 (or R8).
- When R7 (or R8) is changed to adjust VG, R3 (=R4) = R9 (=R10) must be set to ensure V_N balance.

R11, R20 : (R12, R21) Bootstrap resistors
- The quiescent current is set by these resistors 4.7kΩ + 4.7kΩ. It is recommended to use this resistor value.

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R15 : Resistor for ripple filter
· (Limiting resistor for predriver TR at the time of load short)

R14 : Used to ensure plus/minus balance at the time of clip.

R18, R19 : Resistor for ripple filter
· When muting TR11 is turned ON, current flows from ground to $-V_{CC}$ through TR11. It is recommended to use 1kΩ (1W) + 1kΩ (1W) allowing for the power that may be dissipated on that occasion.

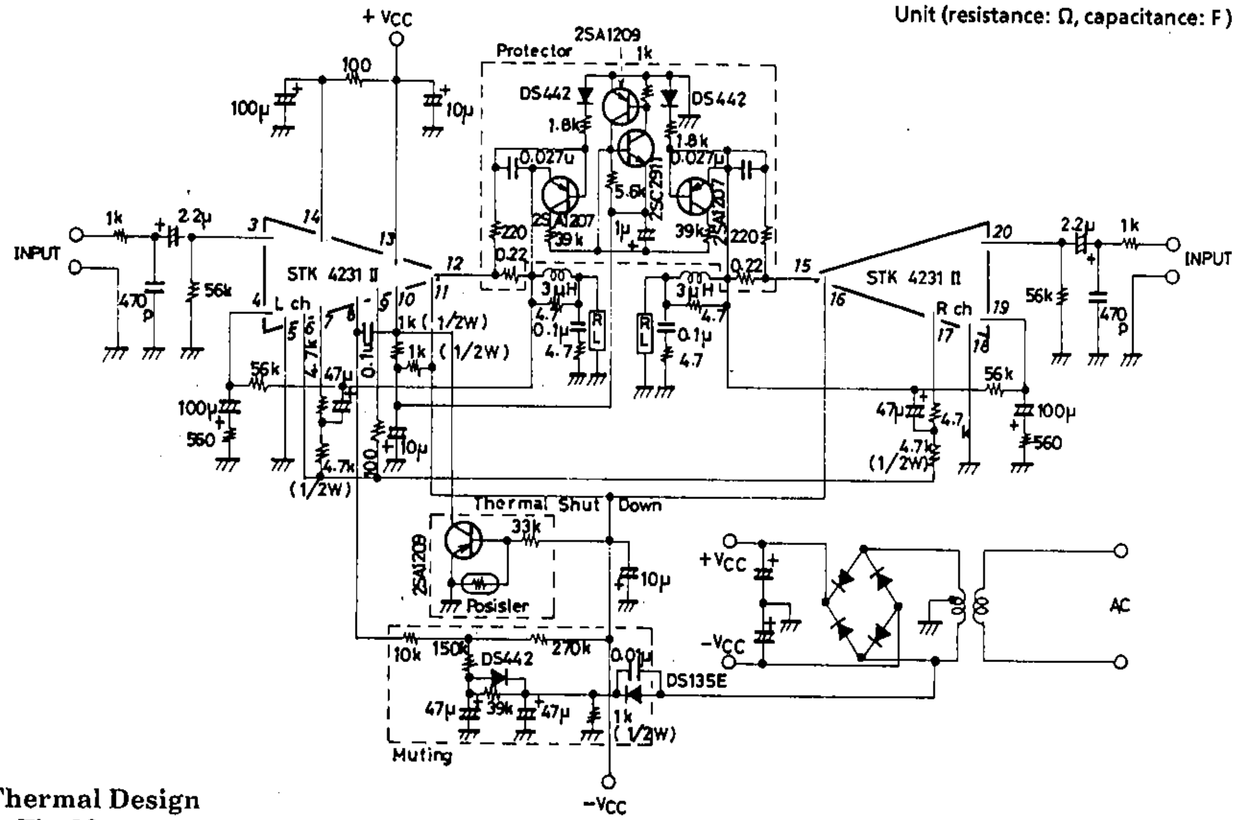
R24, R25 : Oscillation blocking resistors

R16, R17 : Output limiting resistors

R22, R23 : For high-frequency oscillation blocking
L1, L2 :

Sample Application Circuit (protection circuit and muting circuit)

Unit (resistance: Ω, capacitance: F)



Thermal Design

The IC power dissipation of the STK4231II at the IC-operated mode is 137W max. at load resistance 8Ω (simultaneous drive of 2 channels) for continuous sine wave as shown in Fig.1 .

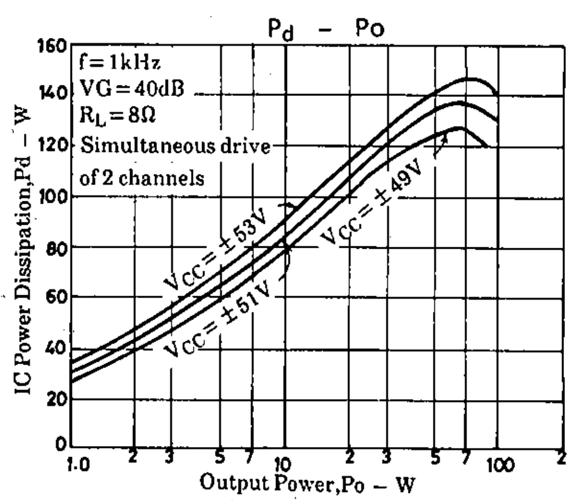


Fig.1 STK4231II Pd – Po (R_L = 8Ω)

In an actual application where a music signal is used, it is impractical to estimate the power dissipation based on the continuous signal as shown above, because too large a heat sink must be used. It is reasonable to estimate the power dissipation as 1/10 Po max. (EIAJ).
That is, Pd = 86W at 8Ω
Thermal resistance θc-a of a heat sink for this IC power dissipation (Pd) is fixed under conditions 1 and 2 shown below.

Condition 1 : $T_C = Pd \times \theta c\text{-}a + Ta \leqq 125°C$ ······· (1)
where Ta : Specified ambient temperature
T_C : Operating case temperature

Condition 2 : $Tj = Pd \times (\theta c\text{-}a) + Pd/4 \times (\theta j\text{-}c) + Ta \leqq 150°C$ ······· (2)
where Tj : Junction temperature of power transistor

Assuming that the power dissipation is shared equally among the four power transistors (2 channels × 2), thermal resistance θj-c is 1.1°C/W and

$$Pd \times (\theta c\text{-}a + 1.1/4) + Ta \leqq 150°C \cdots\cdots (3)$$

Thermal resistance θc-a of a heat sink must satisfy inequalities (1) and (3).
Fig.2 shows the relation between Pd and θc-a given from (1) and (3) with Ta as a parameter.

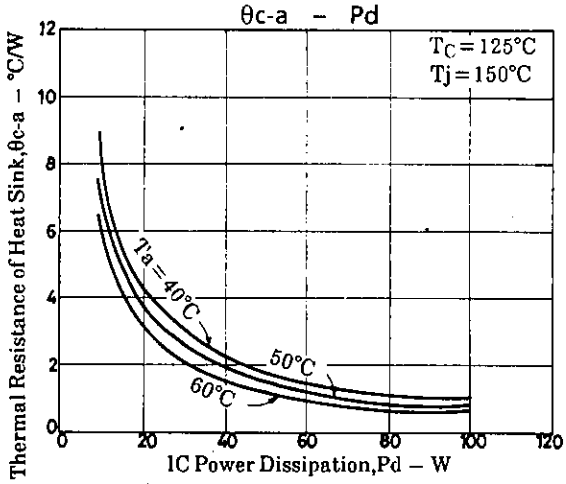


Fig.2 STK4231II θc-a – Pd

[Example] The thermal resistance of a heat sink is obtained when the ambient temperature specified for a stereo amplifier is 50°C.
Assuming $V_{CC} = \pm 51.0V$, $R_L = 8\Omega$,
$R_L = 8\Omega$: Pd = 86W at 1/10 Po max.
The thermal resistance of a heat sink is obtained from Fig.2.
$R_L = 8\Omega$: θc-a = 0.87°C/W
Tj when a heat sink is used is obtained from (3).
$R_L = 8\Omega$: Tj = 148.5°C